

Solutions for Assignment - 5

Important point:

Solutions can be different according to the individual assumptions

1. A trash incinerator has an effective stack height of 100 m. On a sunny day with a 2 m/s wind the concentration of sulfur dioxide 200 m directly downwind is measured at $5.0 \times 10^{-5} \text{ g/m}^3$. Estimate the mass release rate (in g/s) of sulfur dioxide from this stack. Also estimate the maximum sulfur dioxide concentration expected on the ground and its location downwind from the stack.

Solution:

This is a continuous release. For a sunny day a wind stability class A with wind velocity 2 m/s can be assumed. The ground concentration directly downwind for that condition is given by

$$C(x,0,0) = \frac{Q}{\pi \sigma_z \sigma_y U} \exp \left[-\frac{1}{2} \left(\frac{H}{\sigma_z} \right)^2 \right]$$

In a rural area for the stability class A the dispersion coefficients are obtained from Table-2 at page .

$$\begin{aligned} \sigma_y &= 0.22 X(1+0.0001X)^{-0.5} \\ &= 0.22 \times 200 \times (1+0.0001 \times 200)^{-0.5} = 43.56 \text{ m} \end{aligned}$$

$$\begin{aligned} \sigma_z &= 0.20 X \\ &= 0.20 \times 200 = 40 \text{ m} \end{aligned}$$

From the equation we obtain:

$$5 \times 10^{-5} \frac{\text{g}}{\text{m}^3} = \frac{Q_m}{3.14 \times 43.56 \text{ m} \times 40 \text{ m} \times 2 \frac{\text{m}}{\text{s}}} \exp \left[-\frac{1}{2} \left(\frac{100 \text{ m}}{40 \text{ m}} \right)^2 \right]$$

$$Q_m = 12.43 \text{ g/s}$$

The location of the maximum concentration is found by:

$$\sigma_z = \frac{H}{\sqrt{2}} = \frac{100 \text{ m}}{\sqrt{2}} \approx 70 \text{ m}$$

Now, the distance x is obtained from:

$$0.2X = 70 \text{ m}$$

$$X = 350 \text{ m}$$

New dispersion coefficients are:

$$\begin{aligned}\sigma_y &= 0.22 X(1+0.0001X)^{-0.5} \\ &= 0.22 \times 350 \times (1+0.0001 \times 350)^{-0.5} = 75.68 \text{ m} \\ \sigma_z &= 70 \text{ m}\end{aligned}$$

The expected max.sulfur dioxide concentration on the ground is estimated by:

$$\begin{aligned}C(\text{max}) &= \frac{2Q_m}{\pi U H^2} \exp\left[\left(\frac{\sigma_z}{\sigma_y}\right)^2\right] \\ &= \frac{2 \times 12.43 \frac{\text{g}}{\text{s}}}{3.14 \times 2 \frac{\text{m}}{\text{s}} \times (100 \text{ m})^2} \exp\left[\left(\frac{70 \text{ m}}{75.68 \text{ m}}\right)^2\right] \\ &= \frac{24.86}{6.28 \times 10^4} \times 2.52 \text{ g/m}^3 = 9.96 \times 10^{-4} \text{ g/m}^3\end{aligned}$$

2. A reactor in a pesticide plant contains 1000 lb of a liquid mixture of 50% by weight liquid methyl isocyanate (MIC). The liquid is near its boiling point. A study of various release scenarios indicates that a rupture of the reactor will spill the liquid into a boiling pool on the ground. The boiling rate of MIC has been estimated to be 20 lb/min. Evacuation of the population must occur in areas where the vapor concentration exceeds ERPG-1 (5 ppm or 12.5 mg/m³). If the wind speed is 3.4 mph on a clear night, estimate the area downwind that must be evacuated.

Solution:

A plume of MIC can form during evaporation of MIC from the boiling pool. From the Table-1, for the wind speed is 3.4 mph or 1.52 m/s and a clear night condition the stability class is F. Using Table-2, in a rural area for stability class F, the dispersion coefficients are given by:

$$\sigma_y = 0.04 X(1+0.0001X)^{-0.5} \quad [1]$$

$$\sigma_z = 0.016 X(1+0.0003X)^{-1.0} \quad [2]$$

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Let X is the location of the maximum concentration. The maximum concentration on ground with release height H=0 is given by:

$$C(x,0,0) = \frac{Q}{\pi\sigma_z\sigma_y U}$$

Here,

$$Q_m = 20 \text{ lb/min} = 151.2 \text{ g/s}$$

Maximum acceptable concentration $C = 5 \text{ ppm}$ or 12.5 mg/m^3 or 0.0125 g/m^3

Now,

$$0.0125 \frac{\text{g}}{\text{m}^3} = \frac{151.2 \frac{\text{g}}{\text{s}}}{3.14 \times \sigma_z \sigma_y \times 1.52 \frac{\text{m}}{\text{s}}}$$
$$\sigma_z \sigma_y = 2534 \quad [3]$$

Using Maple to solve the equations for X, we have,

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> solve( {Sy-0.04*X*(1+0.0001*X)^(-0.5)= 0, Sz-  
0.016*X*(1+0.0003*X)^(-1.0)= 0, Sy*Sz-2534=0}, [Sy,Sz,X]);  
Sy = 102.1274775, Sz = 24.81212758, X = 2899.845562
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Therefore, the downwind distance X is $2899.845 \approx 2900 \text{ m}$ or 2.9 km . The evacuated area is given by:

$$A = \frac{\pi \times X^2}{4}$$
$$= \frac{\pi \times (2.9 \text{ km})^2}{4} = 6.60 \text{ km}^2$$

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3. The EPA Risk Management Plan (RMP) defines a worst-case scenario as the catastrophic release of the entire process inventory in a 10-min period (assumed to be a continuous release). The dispersion calculations must be completed assuming F stability and 1.5 m/s wind speed. As part of the RMP rule, each facility must determine the downwind distance to a toxic endpoint. These results must be reported to the EPA and to the surrounding community.
 - a. A plant has a 100-lb tank of anhydrous hydrogen fluoride (molecular weight = 20). The toxic endpoint is specified in the RMP as 0.016 mg/L. Determine the distance downwind (in miles) to the toxic endpoint for an EPA worst-case release.

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- b. Comment on the viability of using a continuous release model for a 10-min release period.
- c. One hundred pounds of HF is a small quantity. Many plants have much larger vessels on site. Comment on how a larger quantity would affect the downwind distance and how this might affect the public's perception of your facility.

Solution:

a. Downwind distance Determination

Given, a continuous release, stability class F and wind speed 1.5 m/s.

The specified RMP toxic endpoint is 0.016 mg/L or 0.016 g/m³

$$\text{The release rate is: } Q_m = \frac{100 \text{ lb}}{10 \text{ min}} = \frac{453.6 \text{ g}}{10 \times 60 \text{ s}} = 75.6 \frac{\text{g}}{\text{s}}$$

Using Table-2, in a rural area for stability class F, the dispersion coefficients are given by:

$$\sigma_y = 0.04 X(1+0.0001X)^{-0.5} \quad [1]$$

$$\sigma_z = 0.016 X(1+0.0003X)^{-1.0} \quad [2]$$

The maximum concentration will occur at the centerline. So, we have

$$C(x,0,0) = \frac{Q_m}{\pi \sigma_z \sigma_y U}$$
$$0.016 \frac{\text{g}}{\text{m}^3} = \frac{75.6 \frac{\text{g}}{\text{s}}}{3.14 \times \sigma_z \sigma_y \times 1.5 \frac{\text{m}}{\text{s}}}$$
$$\sigma_z \sigma_y = 1003.18 \quad [3]$$

Using Maple to solve the equations for X, we have,

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> solve( {Sy-0.04*X*(1+0.0001*X)^(-0.5)= 0, Sz-0.016*X*(1+0.0003*X)^(-1.0)= 0, Sy*Sz-1003.18=0}, [Sy,Sz,X]);
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[Sy = 58.59255562, Sz = 17.12128767, X = 1576.021400]

Therefore, the downwind distance X is 1576 m or 1.6 km \approx 1 mile.

b. Viability checking:

$$F = \left(\frac{uR_d}{x} \right) = \frac{1.5 \times 10 \times 60}{1576} = 0.57 \leq 0.6$$

Since $F < 0.6$, instantaneous model may be a better choice in order to get more conservative estimation.

- c.** The downwind distance will be increased with the increase of HF quantity. Then more area needs to be evacuated to avoid the exposure with toxic HF.

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4. The emergency coordinator has decided that the appropriate emergency response to the immediate release of a toxic material is to alert people to stay in their homes, with doors and windows closed, until the cloud has passed. The coordinator has also indicated that homes 4000 m downwind must not be exposed to concentrations exceeding 0.10 mg/m^3 of this material for any longer than 2 min. Estimate the maximum instantaneous release of material (in kg) allowed for these specifications. Be sure to clearly state any assumptions about weather conditions, wind speed, etc.

Solution:

For instantaneous release of material, the maximum concentration occurs at the center of the cloud directly downwind from the release.

$$C(x,t,0,0,0) = \frac{Q_{\text{inst}}}{\sqrt{2\pi}^{3/2} \sigma_x \sigma_y \sigma_z}$$

The stability classes are selected to maximize the release of material in the above equation. This requires maximum value of dispersion coefficients which occurs with A stability conditions. This is for daytime conditions with strong solar radiation and a surface wind speed less than 2 m/s. Therefore at 4000m downwind from Table-3 we have the dispersion coefficients are:

$$\sigma_x \text{ or } \sigma_y = 0.18 X^{0.92} = 370.82 \text{ m}$$

$$\sigma_z = 0.60 X^{0.75} = 301.78 \text{ m}$$

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Now, maximum instantaneous release of material (in kg) is obtained by:

$$0.10 \times 10^{-3} \frac{\text{g}}{\text{m}^3} = \frac{Q_{\text{inst}}}{\sqrt{2} \times (3.14)^{3/2} \times 372.82 \text{ m} \times 372.82 \text{ m} \times 301.78 \text{ m}}$$
$$Q_{\text{inst}} = 32653 \text{ g} = 32.65 \text{ kg}$$

5. A tank of Chlorine contains 1000 kg of Chlorine at 50 bar gauge (1 bar = 10^5 Pa). What is the maximum hole diameter in this tank that will result in a downwind concentration equal to the ERPG -1 (1 ppm) at a downwind distance of 300 m. You may consider molecular weight of Chlorine as 71 at 1 atm pressure and 298 K and all liquid chlorine vaporize (vapor release model).

Solution:

Through the hole of the tank, a plume of Chlorine vapor is assumed to be dispersed at a downwind distance of 300 m. The largest plume will occur when the dispersion coefficients are smallest and wind speed is small. This usually occurs with stability class F and a rural release.

Therefore, a stability class F with wind speed 2 m/s in a rural seating is considered.

The maximum concentration on ground with release height $H=0$ is given by:

$$C(x,0,0) = \frac{Q}{\pi \sigma_z \sigma_y U}$$

From Table -2: for the stability class F the dispersion coefficients are obtained by:

$$\begin{aligned} \sigma_y &= 0.04 X(1 + 0.0001X)^{-0.5} \\ &= 0.04 \times 300 \times (1 + 0.0001 \times 300)^{-0.5} = 11.82 \text{ m} \end{aligned}$$

$$\begin{aligned} \sigma_z &= 0.016 X(1 + 0.0003X)^{-1.0} \\ &= 0.016 \times 300 \times (1 + 0.0003 \times 300)^{-1.0} = 4.40 \text{ m} \end{aligned}$$

The downwind concentration in g/m^3 is given by

$$C_{\text{ppm}} = 0.08205 \times \frac{T}{PM} \times \frac{\text{mg}}{\text{m}^3}$$
$$C \text{ in mg/m}^3 = \frac{1 \times 1 \times 71}{298 \times 0.08205} = 2.9 \text{ mg/m}^3 = 2.9 \times 10^{-3} \text{ g/m}^3$$

Now,

$$2.9 \times 10^{-3} \frac{\text{g}}{\text{m}^3} = \frac{Q_m}{3.14 \times 11.82 \text{ m} \times 4.40 \text{ m} \times 2 \frac{\text{m}}{\text{s}}}$$

$$Q_m = 0.95 \frac{\text{g}}{\text{s}} = 0.95 \times 10^{-3} \frac{\text{kg}}{\text{s}}$$

Since the storage pressure is 50 bars which is greater than the atmospheric pressure a choked release will be occurred during chlorine vapour release from the tank.

For choked flow, the release rate is calculated by:

$$Q_{m(\text{choked})} = C_o A P_o \sqrt{\frac{\gamma g_c M}{R_g T_o} \left(\frac{2}{\gamma + 1} \right)^{\frac{\gamma + 1}{\gamma - 1}}}$$

Here,

P_o is upstream pressure, = 50 bar = $5 \times 10^6 \text{ N/m}^2$

M is molecular weight of chlorine = 0.071 kg/mole

R is gas constant, $8.314 \times 10^3 \text{ N-m}^3/\text{Kg-mole-K- s}^2$

T_o is gas temperature, $K=298 \text{ K}$

A discharge area, = ?

γ , Specific heat ratio; for chlorine = 1.3

C_o is Gas discharge coefficient = 1 [assumed]

g_c is 1 kg-m/N- s^2

Q_m minimum release rate from part a = 0.95 g/s

Therefore the area, A is required to produce release rate 37.2 kg/s is given by:

$$0.95 \times 10^{-3} \frac{\text{kg}}{\text{s}} = 1 \times A \times 5 \times 10^6 \frac{\text{N}}{\text{m}^2} \times \sqrt{\frac{1.3 \times 1 \frac{\text{kg-m}}{\text{N-s}^2} \times 71 \frac{\text{kg}}{\text{kg-mole}}}{8.314 \times 10^3 \frac{\text{N-m}^3}{\text{kg-k-s}^2} \times 298 \text{ K}} \left(\frac{2}{1.3+1} \right)^{\frac{1.3+1}{1.3-1}}}$$

$$0.95 \times 10^{-3} = 1 \times A \times 5 \times 10^6 \times 3.60 \times 10^{-3}$$

$$A = 5.3 \times 10^{-8} \text{ m}^2$$

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Maximum hole diameter in the tank:

$$A = \frac{\pi \times d^2}{4}$$

$$d = \sqrt{\frac{5.3 \times 10^{-8} \times 4}{3.14}} \text{ m}^2 = 2.6 \times 10^{-4} \text{ m} = 0.026 \text{ cm}$$

Table-1: Atmosphere stability

Surface wind speed	Day, incoming solar radiation			Night, Cloud cover thickly overcast		Anytime Heavy overcast
	Strong	Moderate	Slight	>1/2 Low clouds	<3/8 clouds	
<2 m/s	*A	A-B	B	F	F	D
2-3 m/s	A-B	B	C	E	F	D
3-5 m/s	B	B-C	D	D	E	D
5-6 m/s	C	C-D	D	D	D	D
> 6 m/s	C	D	D	D	D	D

Table-2: Dispersion co-efficient for plume model

Area	Stability Class	σ_y (m)	σ_z (m)
Rural conditions	A	$0.22X (1+0.0001X)^{-0.5}$	0.20X
	B	$0.16X (1+0.0001X)^{-0.5}$	0.12X
	C	$0.11X (1+0.0001X)^{-0.5}$	$0.08X (1+0.0002X)^{-0.5}$
	D	$0.08X (1+0.0001X)^{-0.5}$	$0.06X (1+0.0015X)^{-0.5}$
	E	$0.06X (1+0.0001X)^{-0.5}$	$0.03X (1+0.0003X)^{-1.0}$
	F	$0.04X (1+0.0001X)^{-0.5}$	$0.016X (1+0.0003X)^{-1.0}$
Urban conditions	A-B	$0.32X (1+0.0004X)^{-0.5}$	$0.24X (1+0.0001X)^{0.5}$
	C	$0.22X (1+0.0004X)^{-0.5}$	0.20X
	D	$0.16X (1+0.0004X)^{-0.5}$	$0.14X (1+0.0003X)^{-0.5}$
	E-F	$0.11X (1+0.0004X)^{-0.5}$	$0.08X (1+0.0015X)^{-0.5}$

Table-3: Dispersion co-efficient for puff model

Area	Stability Class	σ_x or σ_y (m)	σ_z (m)
Rural conditions	A	$0.18X^{0.92}$	$0.60X^{0.75}$
	B	$0.14X^{0.92}$	$0.53X^{0.73}$
	C	$0.10X^{0.92}$	$0.34X^{0.71}$
	D	$0.06X^{0.92}$	$0.15X^{0.70}$
	E	$0.04X^{0.92}$	$0.10X^{0.65}$
	F	$0.02X^{0.89}$	$0.05X^{0.61}$

(Ref: Crowl D.A., Louvar J.F. (2002). "Chemical Process Safety, Fundamentals with Applications)